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SHALLOW-WATER PERFORMANCE OF A PLANING BOAT

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Michigan University

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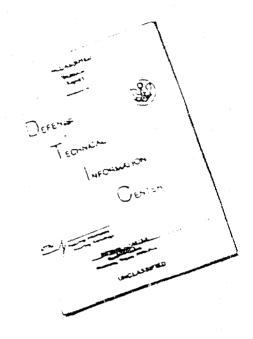
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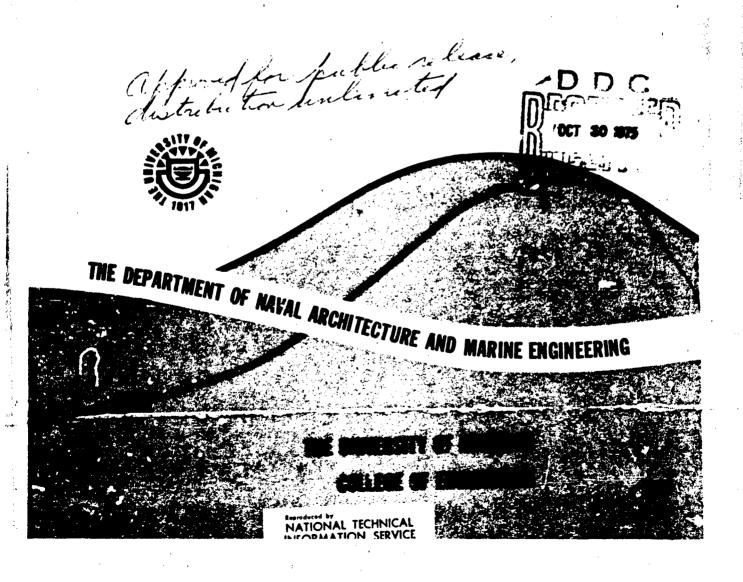
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Andras Istvan Toro



#### SHALLOW-WATER PERFORMANCE OF A PLANING BOAT

by

Andras Istvan Toro

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Student at The University of Michigan

CONTRACT NO. NOO014-67-A-0181-0050

For Presentation at the Annual Meeting of Southeast Section of SNAME April 25, 1969

approved for public release,

#### **ABSTRACT**

The results of a planing-boat model resistance test program conducted at four different water depths, including deep water, and three locations of LCG are presented. The sensitivity of the resistance of a planing boat to shallow water through the critical speed range ( $F_{\rm nh}$  = 0.5-3.5) is analyzed and compared with the deep-water results. Near the critical speed (subplaning), horsepower increases dramatically due to shallowness, but at planing speeds the power is reduced. The paper also gives extrapolated results for a boat of 100,000 lb gross weight. Model and full-scale results are presented in convenient graphical and tabular form for further use.

#### INTRODUCTION .

At the present time, very limited test results which enable a planing-boat designer to approximate resistance in shallow water are available. Several systematic series and the planing-prism data give powering estimates only for deep-water application. Shallow-water data is available only for displacement hulls. However, the resistance of a planing hull in shallow water can be significantly different than in deep water. The greatest effect of shallowness on trim, CG rise, and resistance is at relatively low  $\mathbf{F}_{7}$  or speeds somewhat less than hump speeds, which is the general operating condition where trim, CG rise, and resistance are the most sensitive to speed changes. This is important even for a boat designed to normally operate at relatively high  $\Gamma_{v}$  and in deep water, since the low speeds such a boat would experience would be in channels, rivers, and harbors where the water is shallow.

The need for shallow-water data and the opportunity to investigate an interesting phenomenon led to tests of a Series 62 hull form in four different water depths and at three different LCG locations. The tests were performed at The University of Michigan Ship Hydrodynamics Laboratory in Ann Arbor, Michigan.

#### NOMENCLATURE

Ap	=	Projected planing-bottom area, excluding area of external spray strip, sq ft
B <sub>p</sub>	<b>=</b>	Beam or breadth over chines, exluding external spray strip, ft
B <sub>PA</sub>	<b>=</b>	Mean Breadth over chines: $A_p/L_p$ , ft
B <sub>FT</sub> .	=	Breadth over chines at transom, excluding external spray strip, ft
ВРХ	2	Maximum breadth over chines, exhuding external spray strip, ft
BL	=	Base line
b	<b>=</b> .	Breadth over spray strips at longitudinal location of center of gravity, ft
CL .	=	Centerline
CG .	=	Center of gravity
c <sub>T</sub>	=	Total resistance coefficient
$c_R$	=	Residual resistance coefficient
h .	=	Finite depth of water, ft
$\mathbf{F}_{\mathbf{n}}$	=	Froude number based on length

Nomenclature used is ITTC Standard Symbols and that recommended in SNAME T & R Bulletin 1-23.

F<sub>nh</sub> = Froude number based on finite depth

F<sub>V</sub> = Froude number based on volume

g = Acceleration of gravity, ft/sec<sup>2</sup>

LAV = Average wetted length, ft

LCG = Longitudinal center of gravity

Lp = Projected chine length, ft

L/D = Lift-drag ratio

P<sub>E</sub> = Effective horsepower

R<sub>TM</sub> = Total Model resistance, lb

R<sub>TS</sub> = Total full-scale resistance, lb

 $R_R/\Delta$  = Residual resistance-weight ratio

 $R_{TS}/\Delta$  = Total full-scale resistance-weight ratio

R<sub>Rh</sub>/R<sub>R</sub> = Shallow-water residual resistance-deep-water residual resistance ratio

 $RISE/V^{1/3}$  = CG rise coefficient

S = Wetted surface, sq ft

 $S/V^{2/3}$  = Wetted surface coefficient

v<sub>u</sub> = Velocity of wave propagation, ft/sec

V<sub>K</sub> = Velocity of ship, knots

v <sub>M</sub>	=	Velocity of model, ft/sec
V//L	*	Speed-length ratio
<b>a</b> .	<b>=</b>	Angle of attack at after portion of planing bottom, degrees
<b>λ</b>	٠, •	scale ratio, model to ship
$\lambda_{\mathbf{W}}$	=	Wavelength, ft
β	2	Deadrise angle of planing bottom, degrees
ρ	<b>=</b>	Mass density of water
ν	2	Kinematic viscocity
▼ .	=	Volumetric displacement at rest, cu ft
V/A <sub>p</sub> h		Mean draft-water depth ratio

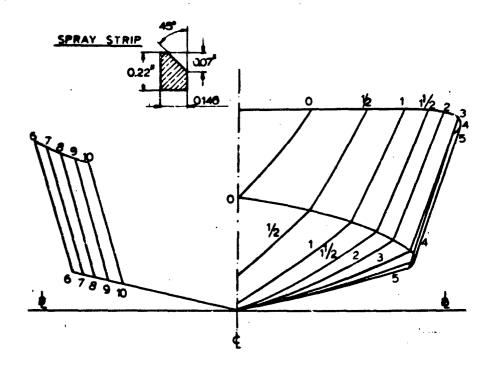
#### DESCRIPTION AND SCOPE OF THE TESTS

As mentioned previously, a Series 62 hull form  $(L_p/B_{px} = 3.06)$  was selected (see Figure 1), as a representative planing hull form.

#### Particulars of the Model No. 1174

A <sub>p</sub> , ft	=	3.322	-	B <sub>PX</sub> /B <sub>P</sub>	= 1.21
L <sub>p</sub> , ft	=	3.50		B <sub>PT</sub> /B <sub>PX</sub>	= 0.71
B <sub>PA</sub> , ft	2	0.949		Centroid of Ap, %	
B <sub>PX</sub> , ft	=	1.144		Lp Forward of Transom	= 48.2
B <sub>PT</sub> , ft	=	0.810			
L <sub>P</sub> /B <sub>PA</sub>	=	3.69			•
L <sub>P</sub> /B <sub>PX</sub>	' <b>=</b>	3.06	•		

The model was made of wood (sugar pine) and plastic spray strips were fitted on the hull as described in Reference [1], for details see Figure 1. The surface of the model was varnished, and for stimulating turbulent flow, a trip wire 0.035 inches in diameter was fitted on each side of the stem as described in Reference [1], also see Figure 1 for details. On the outside surface of the model, every station and half-station were marked for reading the solid-water wetted length and for obtaining wetted surface.



MODEL Nº 1174

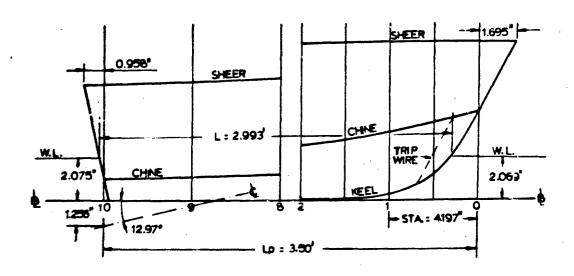


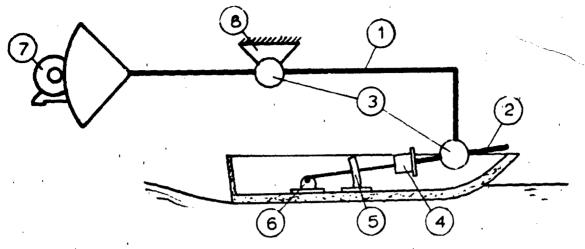
FIGURE 1

A new multilever testing apparatus (Figure 2) was used to measure the towing force on the propeller shaft centerline. The apparatus automatically adjusted by a servo-system to coincide with the shaft line during each run. A switch was attached in the bottom of the model and set for the correct shaft inclination in the static condition. This was the neutral position of the switch, at which time no current was flowing. The tow rod acted as the sliding part of the switch. Whenever the hull trimmed up or down to a new running position, the switch moved out of its neutral position, thereby completing the servo-motor curcuit. The purpose of the motor was to drive the pivoting upper frame to the correct shaft position, at which time the servo-switch became neutral again.

Sinkage and trim were recorded from the same apparatus. For determining wetted surface and wetted length, photographs were taken (see Appendix).

The location of the longitudinal CG is defined as the distance of the LCG from the centroid of the area  $A_p$ , expressed as a percentage of the length  $L_p$ . For the tests, 2%, 6%, and 10% were used.

The shall ow-water depths were chosen to be 7.5, 12.0, and 20.0 inches model scale. In order to relate the shallow-water depth (h) to the boat geometry, a new nondimensional



MULTI-LEVER TESTING APPARATUS

- 1. Pivoting upper frame.
- 2. Rotating lower frame.
- 3. Angle measuring pots.
- 4. Force measuring device.
- 5. Servo-switch.
- 6. Tow point.
- 7. Servo-motor.
- 8. Fix attachment to carriage.



FIGURE 2

parameter is used,  $\nabla/A_{\rm p}h$ . The mean draft-water depth parameter is independent of LCG position. The values of  $\nabla/A_{\rm p}h$  were 0.157, 0.098, and 0.059, respectively, for decreasing water depth.

The length of the adjustable shallow-water bottom in the model basin is 90 feet. Variation of the bottom was ±1/3 inch. There was considered to be no leakage since the bottom was newly installed and made of rigid fiberglass panels.

#### TEST RESULTS

in the Appendix. The resistance data for all conditions have been expanded to a boat gross weight of 160,000 lb. This weight represents a somewhat large-sized motor yacht with a length of approximately 60 feet. The ATTC friction coefficients were used with zero correlation allowance.

Figures 3, 4, and 5 compare model values of resistance, trim, and CG rise at four water depths with each at the same LCG location. The effect of shallowness is evident by simple observation.

Considering the shallow-water phenomenon in more detail for a boat moving in water of restricted depth but unrestricted width at  $F_{\rm hh} \simeq 1.0$ , the water passing under the hull must speed up more than in deep water, which causes reduction in the pressure gradient and an increase in resistance with greater sinkage and trim. The shallower the water depth, the more pronouned is the effect.

The case with the least clearance under the transom was at the 10% LCG location and in 7.5 inches of water. At the critical speed (near  $F_{\rm nh}$  = 1.0) the clearance was approximately 4.0 inches under the transom. In these conditions the water will not flow underneath the hull as easily as in deep water. The flow goes around the hull and sets up a different wave pattern, which is the other important shallow-water phenomenon. As explained in Reference [2], on page 320, the wave pattern follows the law of dispersion of gravity waves.

The velocity of surface waves is given by

$$v_W^2 = \left(\frac{g\lambda_W}{2\pi}\right) \tanh \frac{2\pi h}{\lambda_W}$$
 (1)

For shallow water (h small),

$$\tanh \frac{2\pi h}{\lambda_W} = \frac{2\pi h}{\lambda_W} \tag{2}$$

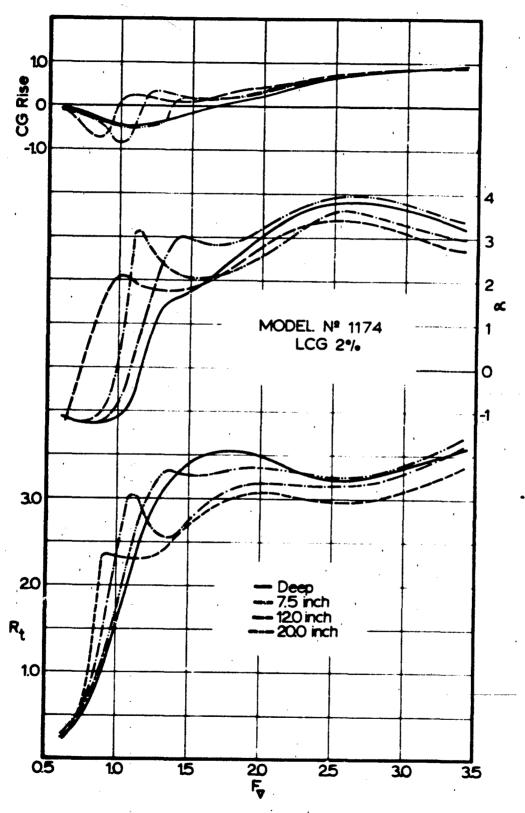


Figure 3

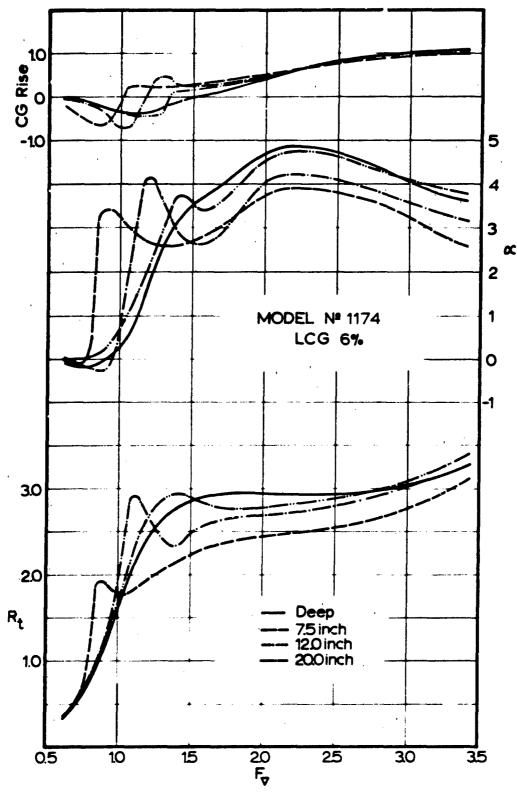


Figure 4

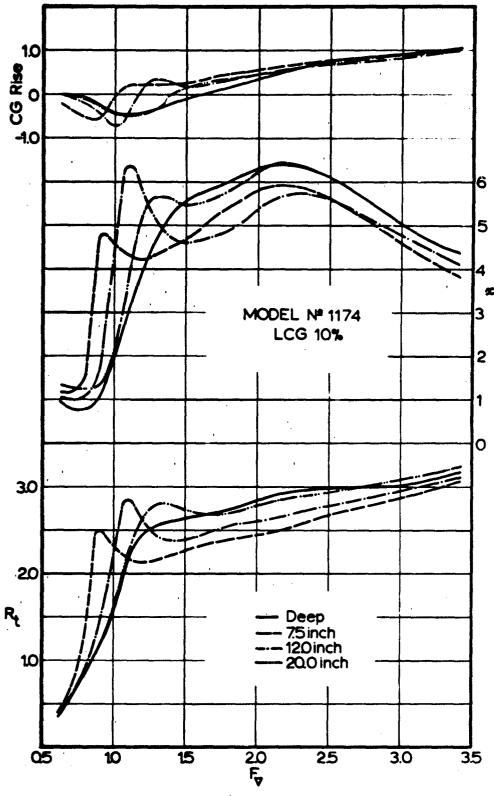


Figure 5

and

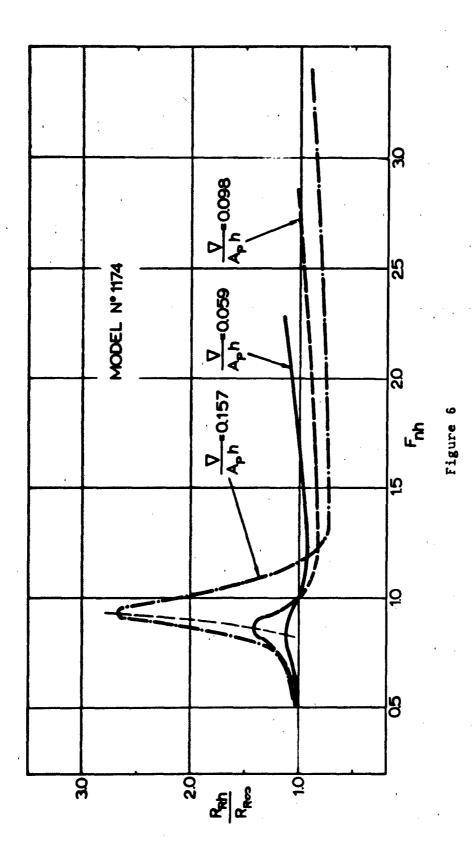
$$v_{u} = \sqrt{gh}$$
 (3)

or

$$F_{nh} = 1.0$$
 (4)

This means that for  $F_{nh}$  = 1.0 the free waves generated by the boat travel with it and appear to form abreast of the boat. That is, the usual Kelvin angle is nearly 19°. At lower speeds (subcritical) the waves are oriented in the usual manner with an angle of 90° 28°. At higher speeds (supercritical) the waves tend to reorient themselves to angles less than 90°, depending on speed. These different wave formations may be expected to represent wave energy losses different than in shallow water, hence alterations in wave resistance. The critical speed is when the residual resistance is greatest (Figure 6).

Because of the trim-sensitive nature of planing boats, and their proportionality between angle of attack and induced drag, one can see how shallowness causes sudden increases in resistance and sinkage. The trend of the shape of all curves is to slowly converge to that of the deep-water condition as  $\nabla/A_n h \to 0$ .



It is interesting to note that the curves in Figure 6 for each value of  $\nabla/A_ph$  are drawn through the data for all LCG's, there being little variation due to LCG, even though one might anticipate otherwise from the previous reasoning. However, for each curve both the  $R_{Rh}$  and  $R_{Ro}$  on the ordinate scale in Figure 6 are taken for the same LCG. Therefore, the change in angle of attack is not influenced by LCG position for a given shallowwater depth.

On Figure 6, in the supercritical region the curves drop below  $R_{Rh}/R_{R\infty}=1$ , representing a power savings. Indeed, that phenomenon is also governed primarily by  $F_{nh}$  and secondarily by  $\nabla/A_{ph}$ . In this supercritical domain, the local flow contributes to greater dynamic lift, which is also shown by the sinkage curves. Eventually all curves in Figure 6 go above  $R_{Rh}/R_{R\infty}=1$  at high  $F_{nh}$ , at which time the adverse wave formations again become dominant.

Presentation of power curves was necessary for practical application. In Figures 7 and 8,  $P_{\rm E}$  (effective horsepower) is plotted against  $V_{\rm K}$  (speed in knots), holding the water depth constant and showing the power variation with LCG locations. In shallow water the optimum LCG position does not seem to vary significantly from

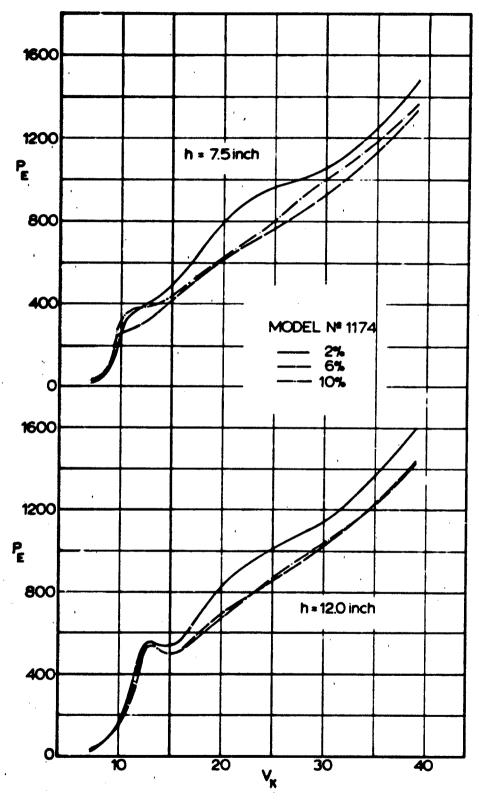


Figure 7

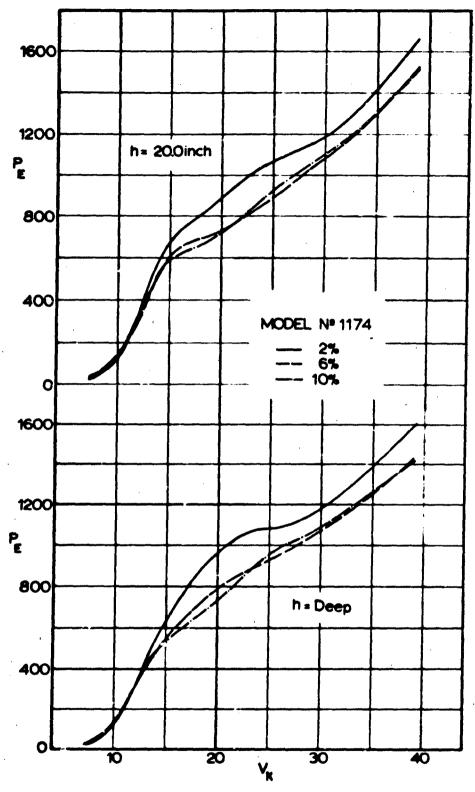


Figure 8

what the deep-water results show. At critical speeds, power may be increased by a factor of two or more, while at supercritical speeds power reductions of 10%-15% may be anticipated.

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  Sharma, The University of Michigan, College of Engineering, Department of Naval Architecture and Marine Engineering, Winter Term 1969.

APPENDIX

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. 10	•••	-		اد	0	85.83	40.12	23.58	11.33	7.44	7.36	8.50	1.03	9.35	7.00	7.64	7.46	7.40	7.46	7.53	7.82	6.01	6.13	7.97	7.77	7.91
CENTRAL	NOUCHHEES ALLONANCE	¥	1	RISE	$\Delta_{\uparrow}$	-0.016	-0.027	-0.042	-0.093	-0.094	0.001		6.633	0.024	0.019	0.022	0.027	0.036	9.04	050.0	0.00	0.030	6.093	0.103	9.106	0.109
SHIP DISPLACEMENT	N SSEME	PRICTION LIM		S	$\Delta$	7.266		7.67	7.56	7.41	7.27	7.00	16.91	6.78	6.63	6.49	6.36	6.23	6.11	9.38	5.73	5.40	Н	1 4.95	4:72	6.69
		Par.		σ١	<b>4</b> 2	26.1	65.1	126.5	296.2	501.3	557.1	526.9	548.9	625.7	709.7	701.1	849.5	907.4	950.2	996.	0.097 1049.6	0.090 1116.0	0.085 1192.8	0.003 1310.5	0.003 1439.6	0.064 1589.7
	_	-01x0		R	V		0.020	6.037	0.001	0.126	0.136	0.106	0.10	0.10	0.110	0.112	0.113	0.113	0.110	0.106						
68.0.7	1.9364	u : 0.10806x10-4	- 12.0 in.	RTS	0	0.012	0.025	0.042	0.088	0.134	0.136	0.110	0.113	0.120	0.127	0.131	0.134	0.135	0.134	0.133	0.128	0.125	0.123	0.126	1 0.129	0.133
TEMPERATURE :	-	3	DEPTH	ပ	¥	5.650	9.704	6.131	6.233	0.300	0.253	0.184	0.151	0.139	0.130	0.119	0.109	9.880	8.807	7.870	6.220	5.073	7.271	3.810	3.455	3.228
TEMPE		•	MATER	Ç	1-01×	0.100	0.139	6.173	0.276	0.340	0.292	0.223	0.190	0.178	0.160	0.157	0.147	0.136	0.125	0.115	9.907	8.723	7.898	7.420	7.049	6.011
	3.50 ft			A,	<u>√</u> 4	1165.1	2492.5	4240.7	8824.0	13439.9	13577.0	11772.5	11321.2	11983.2	12684.7	13088.4	13397.7	13516.0	13409.3	13072.1	12791.3	12476.6	12300.6	12549.0	12865.8	13319.4
ON 1 28		. 16.84		i	5	0.282	0.329	111.0	0.434	0.471	1.740 0.518	0.565	15.79 2.057 0.612	0.060	0.706	0.754	108.0	0.848	0.895	0.942	26.72 3.481 1.036	1.130	1.225	4.431 1.319	1.413	18.87 5.064 1.507
L.C.G. LOCATION	ENGTH	WTIO		>[	7	7.29 0.945	6.50 1.107	9.71 1.266 0.377	1.424	12.14 1.592		14.57 1.898	2.057	17.00 2.215	18.22 2.373	19.43 2.532	20.65 2.690 0.801	21.86 2.848	23.08 3.006	9 3.165	2 3.481	5 3.797	8 4.114		4 4.747	7 5.06
.6.0.	MODEL LENGTH	SCALK RATIO		>,		L			10.93	L	13.36						$\vdash$			1 24.29	۵. ـ	29.15	31.58	34.01	16.44	
-	•	•			ਤੇ <i>ਦ</i>	3.52	3.62	3.63		3.40	3.30	3.21	3.14	3.08	3.02	2.92	2.91	2.85	2.78	2.74	2.60	2.50	2.39	5 2.28	2.18	3 2.08
		1963		S	733	3.45	3.60	3.64	3.60	3.52	3.45	3. 16	3.28	3.22	3.15	3.08	3.02	2.96	2.90	2.84	2.72	2.60	2.67	2.35	2.24	2.13
1174	2-13	: 22 Feb. 1969		CG	1. 1		22	35	11	78	<b>90.</b> +	+.36	• . 28	4.20	• 16	• . 10	4.22	+.30	+.40	•••	+.67	+.72	1.77	•.85	•••	+.90
		- 7		χ	RISE Hayres Inch	-1.13	. 597 -1. 23	-1.13	. 53	1.57	3.07	2.57	2.27	2.07	2.07	2.17	2.27	2.37	2.62	2.82	3.37	3.62	3.52	3.39	3.12	3.97
MODEL NO. :	TEST NO.	DA'FK		R	Σ 2	Se		. 978	1.952	5.00 2.904	2.96	6.00 2.620	2.557	1.00 2.723	2.897	8.00 3.012	8.50 3.107	9.00 3.163	9.50 3.178	10.00 3.184	11.00 3.151	17.00 3.162	13.00 3.192	14.00 3.309	15.00 3.440	16.00 3.596
*	+	S		>	S &	3. 00.	3.50	4.00	4.50	2.00	\$.50	6.00	6.50	1.00	1.50	8.00	8.50	9.00	9.50	10.00	11.00	17.00	13.00	14.00	15.00	16.00

				5	\$	E.	\$	:	<b>~</b>	.750	=	=	. 954	1.023	1.001	1.159	1.227	1.295	1.364	1.500	1.636	1.773	1.909	2.046	2
4			L	_	•	•	•	•	•	•		•	ŀ	=	E	=	: T	7.1	-	E	-	E	E	Ē	7:10
1 100,000 1b	• . 000	A.T.T.C.	L		6.637	0.743	0.049	9.955	1.062	7.92 1.168	1.274	1.380	1.436	1.592	1.699	1.805	116.1	2.017	2.123	2, 336	2.548	2.761	2.973	3.185	3, 3'13
2	•	: <b>A</b> .	٦	۵	19.6	47.54	28.40	15.36	10.30	7.92	6.9	6.64	6.77		6.91	6.83	69.9	7.00	7.10	7.42	7.68	7.70	7.66	7.44	7.24
CENTRAL	LLOMANC	Y	RISE	ξĎ	-0.012	-0.020	-0.036	7.67 -0.051	-0.060	7.37 -0.058	-0.051	0.012	0.024	0.024	0.023	0.025	0.030	0.042	0.055	0.075	0.085	0.094	0.103	0.109	0.115
SHIP DISPLACEMENT	HOUGHNESS ALLONANCE	FRICTION LINE	S	Δŧ	7.27	7.50	1.71	7.67	7.54	7.37	7.10	6.9	6.76	6.59	.40	6.23	6.11	6.13	5.79	5.54	5.27	\$.05	4.8	4.63	4.46
<b>SH1</b>	90	FRIC	ď		25.0	54.9	105.1	216.5	362.2	517.7	640.1	729.9	771.4	613.0	163.9	920.7	9.4.8	0.118 1012.3	0.115 1050.4	0.105 1106.6	1164.9	0.091 1247.1	0.089 1363.9	0.089 1503.9	0.089 1648.4
	_	0.10808x10 <sup>-4</sup> 20.0 in.	RR	V	0.00	0.016	0.029	0.058	0.08	9.116	0.131	0.137	0.133	0.129	0.126	0.125	0.123	L			0.097		0.089	<u> </u>	
60.03	1.9364	: 0.10808x	$R_{TS}$		0.011	0.021	0.035	90.0	0.097	0.126	0.143	0.151	0.148	0.145	0.145	0.145	0.145	0.143	0.141	0.135	0.130	0.129	0.131	0.134	0.138
TEMPERATURE : 60.0°F	•	u DRPTH	۲	x1-01x	5.312	7.845	0.105	0.164	0.207	0.250	0,224	0.205	0.177	0.153	0.136	0.122	0.110	0.946	8.800	6.954	5.656	4.734	4.168	3.793	3.442
TEMPE		WATER	Ċ	×10-1	9.746	0.121	0.146	0.205	0.247	0.269	0.263	0.240	0.216	0.191	0.174	0.160	0.147	0.132	0.125	0.106	9.333	8.380	7.790	7.397	7.028
	3.50 ft	16.84	R	<u> </u>	1115.6	2103.5	3521.3	6510.5	9710.6	12618.4	14301.2	15054.0	14773.1	14532.7	14476.4	14520.6	14519.3	14285.4	14081.4	13485.9	13013.3	1286.0	13059.9	13440.7	13811.2
OM : 28		. 16	LL	<b>.</b>	0.282	0.329	0.377	0.424	0.471	0.518	0.565	0.612	0.660	0.706	0.754	0.801	0.848	0.895	0.942	1.036	1.130	1.225	1.319	1.413	1.507
L.C.G. LOCATION	NODEL LENGTH	RATIO			7.29 0.945	8.50 1.107	9.71 1.266 0.377	10.93 1.424	12.14 1.582	13.36 1.740	14.57 1.898	15.79 2.057	17.00 2.215	18.22 2.373	19.43 2.532 0.754	20.65 2.690 0.801	21.86 2.848	23.08 3.006	24.29 3.165	26.72 3.481	29.15 3.797	31.58 4.114 1.225	34.01 4.431	36.44, 4.747	38.87 5.064 1.507
.c.6.	DEL	SCALE RATIO	>,	٤	1	[				L	i			<b>i</b> 1		1									
	Z	<i>s</i> a	ال	3 #	3.50	3.58	3.64	3.60	3.50	3.40	3.30	3.22	3.15	3.04	2.93	2.85	2.76	2.70	2.63	2.50	2.40	2.32	2.24	2.15	2.07
		1969	S	ft.2	3.45	3.60	3.66	3.64	3.58	3.50	3.41	3.32	3.21	3.13	3.04	2.96	2.90	2.84	2.75	2.63	2.50	2.40	2.30	2.20	2.12
174	3-20	: 22 Feb. 1969	ည	Z 10 27 d	10	17	30	42	50	48	42	+.10	+.20	+.20	+.19	+.21	+.25	+.35	+.46	+.62	+.70	+.78	+.85	+.90	+.95
MODEL NO. : 1174	•	. 2	೪	degree inch	-1.03	-1.23	-1.25	_	-0.33	. 97	2.17	2.87	2.97	2.87	2.83	2.87	3.07	3.27	3.47	3.77	3.97	3.92	3.82	3.62	3.42
ODEL N	TEST NO.	DATE	R	<u> </u>	. 293	.518	.832	1.467	5.00 2.146	2.766	3.137	3.319	7.00 3.289	3.271	8.00 3.290	8.50 3.330	3.364	3.361	3.378	11.00 3.285	12.00 3.253	13.00 3.291	14.00 3.400	3.545	16.00 3.693
Σ	÷		>2	fps	9	3.50		4.50	5.00	5.50	6.00	6.50	7.00	7.50	9.00	8.50	9.00	9.50	10.00	11.00	12.00	13.00	14.00	15.00	16.00

8	NODEL NO. :	1174		ů.	6.	LOCATION	5 . 3		1001	TEMPERATURE :	68.0°F	•	SHIP	BHIP DISPLACEMENT	CENERAL	91 .	100,001	
TEST NO. : 6-00	:			¥	ODEL LENGTŲ	SMCTH.	m ,	3.50 ft		•	1.9364		BOOM	HEES A	NOUGHIESS ALLONANCE	•	0.000	
1 22 1	22	i	22 Pab. 1969	ซั	CALE BATIO	. 0111	• 16	16.84	WATER	- at 120	0.10808x10 <sup>-4</sup> DEEP	-01×	PRIC	PRICTION LINE	#		A.T.T.C.	
8		(Q)	S		>3	>[	L	2	U,	C <sup>t</sup>	A <sub>TS</sub>	R	۵	S	RISE		L	L
degree	<u> </u>	T uch	ft. <sup>2</sup>	3 2			-	<u>√</u> ≅	x10-1	X101x	10	0	۾ لد	<b>\$</b> 2 ∧	fΔ	0		<u>د</u>
-0.1	Н	0	3.35	3.40	7.29	0.945 0.282	0.282	1353.4	13	7.180	0.014	0.010	30.3	7.06	0.0	3.6	0.637	
. 623 -0.2	_	09	3.38	3.41	05.0	8.50 1.107 0.329	0.329	2641.0	0.155	0.112	0.026	0.022	6.6	7.12	-0.011	37.86	0.743	
.876 -0.1	- T	17	3.49	3.45	11.6	1.266 0.377	0.377	3756.0	0.162	0.119	0.038	0.032	112.1	7.35	-0.020	26.62	0.049	
0.15		27	3.53	3.52	10.93	1.424	0.424	6002.9	0.19	0.155	0.060	0.053	201.5	7.63	-0.033	16.66	0.955	
5.00 1.897 0.6		35	3.52	3.55	12.14	1.582 0.471	0.471	8.504.8	0.222	0.182	0.085	0.076	317.2	7.41	-0.042	11.76	1.062	
2.353 1.4		36	3.47	3.52	13.36	1.740 0.518	0.518	10606.9	0.231	0.192	0.106	0.096	435.2	7.31	-0.044		1.168	
6.00 2.583 2.45		5 23	3.39	3.45	14.57	14.57 1.898 0.565	0.565	11599.3	0.210	0.179	0.116	0.104	519.1	7.14	-0.028	8.62	1.274	
2.757 3.10		01 10	3.31	3.36	15.79	2.057	0.612	12311.0	0.203	0.165	0.123	0.110	596.9	6.97	-0.012	6.12	3.380	
2.857 3.5	- 1	0	3.20	3.25	17.00	2.215	0.660	12666.9	0.186	0.149	0.127	0.112	661.4	6.74	0.0	7.89	1.486	
3.75	ויש	\$ +.05	3.10	3.13	18.22	2.373	902.0	12834.3	0.173	0.134	0.128	0.112	718.0	6.53	900.0	7.79	1.592	
8.00 2.964 4.00	Υ	<b>5.14</b>	3.01	3.00	19.43 2.532		0.754	12901.6	0.158	0.120	0.129	0.111	769.9	6.34	0.017	7.75	1.699	
8.50 2.960 4.30	21	023	2.92	2.87	20.65 2.690		0.801	12731.8	0.144	0.107	0.127	0.107	607.3	6.15	0.028	7.65	1.805	
2.956 4.55	ᆲ	5 +.33	2.83	2.76	21.86	2.848	0.848	12564.6	6.133	9.543	0.126	0.104	843.5	5.96	0.040	7.96	1.911	
9.50 2.953 4.75	2,1	5 +.44	2.72	2.63	23.08	3.006	0.895	12414.7	0.124	8.653	0.124	0.101	879.8	5.73	0.053	\$0.0	2.017	
10.00 2.942 4.85	=	5 +.55	2.63	2.54	24.29	3.165	0.942	12220.5	0.115	7.793	0.122	0.097	911.6	5.54	990.0	9.10	2.123	
11.00 2.932 4.80	×۱	0 +.75	2.46	2.38	26.72	3.481	1.036	11895.9	0.101	6.433	0.119	0.091	976.1	5.18	0.091	9.41	2.336	
12.00 2.953 4.70	2	4.89	2.34	2.27	29.15	3.797	1.130	11689.8	9.048	5.335	0.117	0.085	1046.4	4.93	0.108	8.55	2.548	
13.00 3.005 4.45	-1	5 +.945	\$ 2.22	2.17	31.58	4.114 1.225	1.225	11656.8	8.272	4.582	0.117	0.082	0.082 1130.4	4.68	0.114	8.58	2.761	
14.00 3.058 4.10		0 +1.0	2.12	2.10	34.01	4.431	1.319	11616.2	7.601	3.938	0.116	0.078	0.078 1213.1	4.46	0.121	19.8	2.973	
15.00 3.159 3.85	= 1	5 +1.05	\$ 2.05	2.05		4.747 1.413	1.413	11776.3	7.074	3.440	0.118	0.076	0.076 1317.7	4.32	0.127	8.49	3.185	
16.00 3.258 3.00		0 +1.10	1.98	1.97	38.87	5.064	1.507	11915.9	6:93	3.021	0.119	0.073	0.073 1422.2	4.17	0.122	6.39	1, 198	
															1			

_	T <sub>E</sub>	999	.780	5	1.003	1:11	1.236	1.337	1:4	1.560	1.671	1.783	1.894	2.006	2.117	2.229	2.452	2.675	2.897	3.120	3.343	3.566
100,399 115 9.4000 A.Y.T.'.	L <sup>D</sup>	0.637	0.743	6.83	6.6.9	1.062	1.168	1.274	7,380	1.1.16	1.592	1.699	1.805	1.911	2.017	2.123	2.116	2.518	2.761	2:473	3.135	1. 1.3
		66.81		_	70.21	12.59	11.72	11.27	10.84	10.37	10.13	10.06	9.95	10.00	9.98	10.04	10.09	10.05	9.86	9.66		96.8
CEMENT LLOMANCI NR	RISE V3	-0.029	-0.060	0.080	0.0	0.0	0.028	0.025	J		0.039	1	0.048	0.054	090.0	0.066	0.085	0.100	0.105	0.112	0.115	0.118
SHIP DISPLACEMENT ROUGHNESS ALLOMANCE. PRICTION LINE	S	7.16	7.42	7.43	7		7.03		6.6	6.49	6.32		5.85	5.62	5.47	5.33	5.05	4.80	4.57	4.32	4.15	4.04
SHIP	5 س⊅	33.5	0.69	257.9	278.0	- }	350.1	397.0	447.2	503.4	552.0	593.5	637.2	671.0	710.3	743.0	013.0	890.4	983.3	1081.4	0.067 1206.2	0.067 1331.6
**10-4	R <sub>R</sub>	0.012	0.022	0.001	- 1	- 1	0.075	0.077		0.082	0.083	0.082	0.081	0.079	0.078	0.076	6.072	0.069	0.067	0.066		i
68.0°F 1.9364 0.10808x10 <sup>-6</sup> 7.5 in.	St. \	0.015	0.027	- 1	- 1	0.079	0.085	0.089	0.092	0.096	660.0	0.100	0.100	0.100	0.100	001.0	660.0	0.100	0.101	0.104	0.108	0.112
TEMPERATURE : 68.0°F p : 1.9364 p : 0.1080 ATER DEPTH = 7.5 in.	ا م	8.037	0.108	0.300	0.226	0.175	0.157	0.139	0.124	0.114	0.102	9.262	6.519	7.719	6.987	6.290	5.200	4.406	3.860	3.472	3.174	2.845
TEMPER	7_1-8	12:	0.153	0.342	0.267	0.216	0196	0.178	0.163	0.152	0.141	0.130	0.123	0.115	0.107	0.100	8.948	8.129	7.556	7.151	6.834	6.476
5.50 ft 16.84	A TS	1496.7	2674.9	8643.7	8283.2	7944.0	8533.9	8869.5	9222.5	9640.0	9866.9	9945.0	10049.4	9995.3	10033.7	9960.5	9907.7	9946.9	10139.5	10355.9	10780.2	11157.2
	LE	0.282	0.329	1.266 0.377	0.424	1.582 0.471	1.740 0.518	0.565	2.057 0.612	2.215 0.660	2.373 0.706	0.754	0.801	2.848 0.848	0.895	0.942	1.036	3.797 1.130	4.114 1.225	1.319	4.747 1.413	1.507
.G. LOCATION EL LENGTH LE RATIO	>[긪	0.945	8.50 1.107			- 1		4.57 1.898 0.565	2.057			2.532	0.65 2.690	2.848	3.006	3.165	3.481			4.431		5.064
L.C.G. MODEL L	> <sub>x</sub>	7.29				<b>-</b> 1	13.36	1	15.79	17.00	18.22	19.43	~	21.86	23.08	5 24.29	\$ 26.72	1 29.15	31.58	34.01	7 36.44	38.87
		3.43	3.48	3.56	3.55	3.47	3.40	3.30	3.20	3.10	0 2.98	2.86	8 2.73	7 2.61	0 2.52	3 2.45	2.35		7 2.15	6 2.05	7 1.97	2 1.93
1961	N 2		3.52	3.53	3.47	3.40	3.34	3.25	3.17	3.08	3.00	2.90	2.78	3 2.67	2.60	5 2.53	2.40	3 2.28	7 2.17	3 2.06	5 1.97	1.92
: 1176 : 6-75 : 15 Pob. 1969	O Hand	7	50	66	9:-	+.25	+.23	+.21	+.24	+.29	+.32	+.35	• • •	4.45	5 +.50	4.55	4.70		L	+.93	56.+ 6	86·+ C
	8	05	1	+3.2	4.50 1.822 +3.40	+3.0	5.50 1.925 +2.70	+2.62	_	7.00 2.233 +2.70	+2.85	8.00 2.353 +3.10	+3.35	6 +3.60	1 +3.75	3 +3.90	2.516 +3.90	+3,80	3 +3.60	14.00 2.783 +3.30	2.933 +2.90	16.00 3.082 +2.60
MODEL NO. TEST NO. DATE	<b>2</b> <sup>2</sup> <sup>2</sup> 3	.370	.633	1.872	1.022	5.00 1.778	1.925	6.00 2.02	6.50 2.12	2.233	7.50 2.309	2.353	8.50 2.400	2.415	9.50 2.451	2.468	2.516	12.00 2.584	2.683	2.783	2.933	3.08
Z + O	> <sub>2</sub> §	3.00	3.50	4.00	.50	5.00	5.50	6.00	6.50	7.00	7.50	.00	8.50	9.00	9.50	10.00	11.00	12.00	13.00	14.00	15.00	16.00

							•	•	TEMP	TEMPERATURE : 68.0"F		_		sair displacment		=	110,000	•
	-	6-13		¥	NODEL LI	EL LENGTH	ë	3.50 ft			1.9364	,		1 55 MIR	NOUGHIESS ALLONANCE	•	••••	
	1 22	22 Feb. 1969	1961	Š	SCALE N	RAT10	1 16.84	•	WATE	HATER DEPTH -	: 0.10808x10 <sup>-6</sup> - 12.0 in.	0x10 <sup>-4</sup>	PRIC	PRICTION LING	#		A.T.T.C.	
	S S	ပ္ပ	S		>3	>[	L	2	لٰ	ပ	R	RR	۵	S	RISE		ц	L
	degree inch		ft.2	है द	<		=	2 4	1-01x	X10-1		V	۾ لنا	ξΔ	ξĎ	۵	<b>D</b>	두
	00.	00	3.35	3.42	7.29	.29 0.945	0.282	1579.7	0.132		0.016	0.013	35.4	7.06	-0.009	63.30	0.637	0.520
	15	15	3.45	3.46	8.50	. 50 1.107	0.329	2447.3	0.143	9.982	0.025	0.030	63.9			40.00	6.73	919.
	35	27	3.53	3.52	9.71	1.266	0.377	4239.0	0.178	0.136	0.042	0.037	126.5			23.59	9.65	20.
	00.	60	3.53	3.50	10.97	1.424	0.424	6987.0	0.225	0.184	0.070	0.063	234.5	7.43	-0.062	14.31	0.955	792
		61	3.47	3.55	12.14	1.582	0.471	11780.7	0.305	0.264	0.110	901.0	439.4	7.31	-0.082	3:	1.062	. 88
	5.50 2.868 +4.00	00.	3.40	3.46	13.36	1.740	0.518	13150.3	0.288	0.248	0.132	0.121	539.5	7.16	0.0	7.60	1.160	.96
	6.00 2.489 +3.80	+.45	3.33	3.37	14.57	1.898	0.565	11151.2	0.214	0.175	0.112	0.100	499.1	7.01	<u> </u>	1.97	1.274	1.056
~~!	6.50 2.355 +3.00	+.30	3.25	3.30	15.79	2.057	0.612	10354.8	411.0	0.130	0.104	0.000	502.1	6.84	0.036	9.66	1.380	1.166
31		÷.25	3.16	3.17	17.00	.00 2.215	099.0	10795.6	0.165	0.126	0.10	0.093	563.7	99.9	L	9.26	1.436	1.232
7	7.50 2.511 +2.65	+: 24	3.10	3.07	18.22	2.373	0.706	11074.7	0.153	0.114	0.110	0.094	612.3	6.52	0.032	9.08	1.592	1.320
'3	42.90	87.4	1.02	2.96	19.43	19.43 2.532	0.754	11320.2		0.103	0.113	0.095	675.5	6.36	0.035	8.83	1.699	1.408
71	_	+.35	2.94	2.83	20.65	0.65 2.690	0.801	11324.5	0:130	9.219	0.113	0.093	738.0	6.19	0.042	6.83	1.805	1.496
긔	9.00 2.691 +3.70	+.42	2.86	2.72	21.86	86 2.848	0.848	11234.9	0.120	0.20	0.112	060.0	754.3	6.02	0.051	. 90	1.91	1.584
1	7:5	-+	2.72	-+	23.08	3.006	0.895	11099.1	0.113	7.525	0.111	0.088	786.5	5.73	<u> </u>	9.01	2.017	1.672
11	-+		2.65		24.29	1.29 3.165	0.942	10986.2	0.105	6.739	0.110	0.085	819.5	5.58	9.068	9.10	2,123	1.76
7		-+	2.47		26.72	26.72 3.481	1.036	11043.8	9.538	5.801	0.110	0.082	906.2	5.20	0.091	9.05	2,336	1.936
7	_		2.36	2.27	29.15	3.797	1.130	11067.0	8.601	4.887	0.111	0.079	9.066	4.97	0.103	9.04	2. 18	2.112
71	-		2.25	2.19	31.58	4.114	1.225	11106.1	7.877	4.193	0.111	0.076	1077.0	4.74	0.111	9.00	2.761	2.288
T	14.003.007 +3.70		2.14	2.15	34.01		1.319	11351.9	7.404	3.757	0.114	0.75	1105.5	15.1	0.117		2.973	2.464
7 [	9			2.03	36.44	6.44 4.747	1.413	11625.7	7.009	3.368	0.116	0.074	1300.8	4.32	0.125	.60	3.185	2.640
∵	3.15	16.00 3.266 +3.15 +1.05	1.98	1.97	38.87	38.87 5.064	1.507	11954.2	6.655	3.037	0.120		0.073 1426.9	4.17	0.127	9.36	3.398	2.116

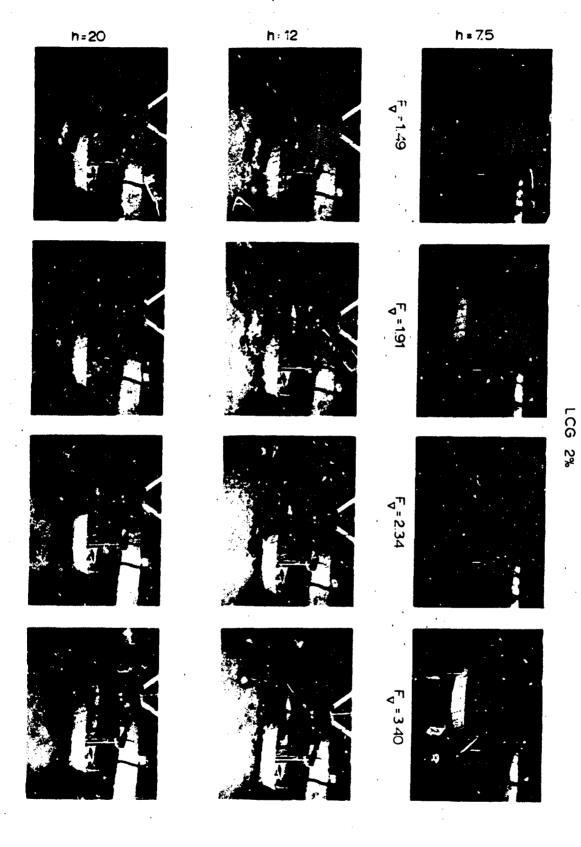
EHIP DISPLACEMENT PRICTION LINE  PRICTION LINE    Columbia   Colum	0.084 1259.0 4.30 0.114 8.30 2.973 1.909 0.083 1384.5 4.13 0.118 8.08 3.185 2.046 0.082 1519.2 4.02 0.123 7.86 3.398 2.182
PRICTION LINE : 10  PRICTION LINE : A.  PRICTION LINE : A.  PRICTION LINE : A.  Decision of the color of the	4.30 0.114 8.30 4.13 0.118 8.08 4.02 0.123 7.86
BHIP DISPLACEMENT:  PRICTION LINE:  PRICTION LINE:  PRICTION LINE:  123.7	4.30 0.114 4.13 0.118 4.02 0.123
11099999	4.30
11099999	
11099999	4 1259.0 3 1384.5 2 1519.2
	4 6 8
A 0.093 0.092 0.092 0.092 0.092 0.092 0.092 0.092 0.093	0.084
20.01 20	0.121 0.124 0.128
MATER DEPTH : 1 10 1 10 0 0 135 0 0 13	4.393 3.962 3.546
MATER HIGH 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	8.072 7.619 7.178
TS 1453.0 ft 1453.0 1453.0 1453.0 1453.0 1453.0 1453.0 1453.0 115	12055.4 12373.5 12729.1
	4.431 1.319 4.747 1.413 5.064 1.507
V.C.G. LOCATION : 1  NLE RATIO : 1	4.431
	36.44
	2.98
13.65 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2	2.04 1.96 1.91
RSE 13.869  1. 23 Feb. 1969  1. 23 Feb. 1969  1. 23 Feb. 1969  1. 24 13 13.46  1. 42 2.75  1. 42 2.75  1. 44 2.2 3.01  1. 42 2.75  1. 44 2.2 3.01  1. 44 2.2 3.01  1. 45 2.75  1. 46 0. 2.55  1. 46 0. 2.55  1. 46 0. 2.55  1. 48 9. 2.75  1. 48 9. 2.	4.15 +.94 3.95 +.98 3.80 +1.02
8 5 11 11 11 11 11 11 11 11 11 11 11 11 1	
PAPEL NO. 1'ES:F NO. 1'ES:F NO. 1 PAFE 1b db 1b	15.00 3.253 15.00 3.253
7 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	15.00

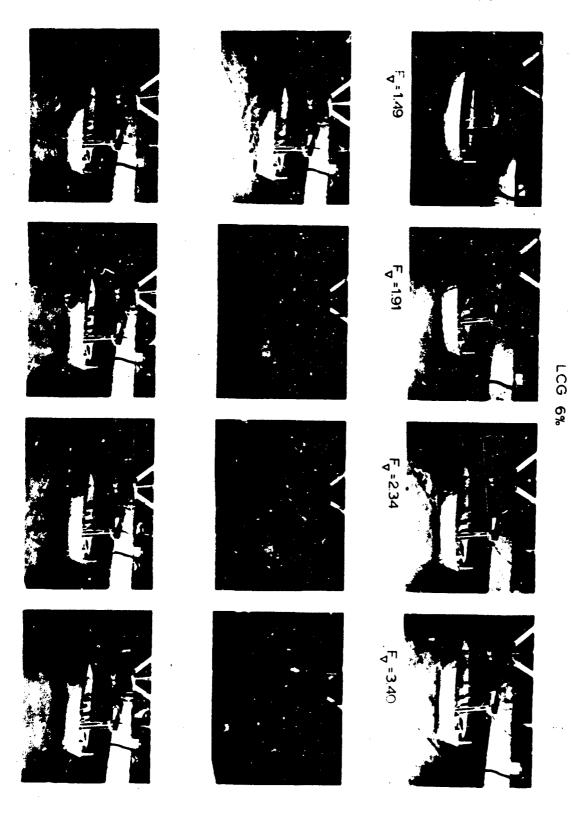
	HODEL	HODEL NO. : 1174	1174		j		C.G. LOCATION	101	•	TEMPE	TEMPERATURE :	68.0°F		AIMS	BHIP DISPLACEMENT	CEMENT	61 :	1100,001	
	T": 110.		10-00		Ī	HODEL LENGTH	MCTH	. 3.	3.50 ft		•	1.9364		BOOC	NOUGHNESS ALLONANCE	LLOWANCE	•	00000	
	DATE	-	22 Pab. 1969	1961	ซั	SCALE RATIO	\T10	1 16.84	***		2	u : 0.10808x10"	Px10-4	FRIC	PRICTION LINE	*		1 A.T.T.C.	
L					ľ					MATER	DEPTH -	DEEP							
> <u>z</u>	<u> کې                                    </u>	8	ပ္ပ	S	7	> <u>×</u>	>[	عنا	حرا	Ç	ပ	RTS	RR	ط		RISE	٦	L	L
*C.	q	dogree inch	Z in	ft. <sup>2</sup>	<b>i</b> #			-	2 4	1-01x	x10-1	Ø	0	۾ لن	V	fΔ	۵	>	بر د
3.00	. 467	7 0.93	04	3.03	3.14	7.29	0.945	0.282	1707.9	13	0.109	0.010	9.014	38.2	6.35	6.36 -6.005	58.55	0.637	T
1.50	50 .719	9 0.73	07	3.06	3.22	05.0	1.107	0.329	3146.5	0.198	0.154	0.032	0.028	1:29	119	-0.008	11:3	0.743	
=	4.001.000	0.8	17	3.25	3.33	9.71	9.71 1.266 0.377	0.377	4398.4	0.198	0.156	0.044	0.039	131.2	9.9	-0.020	22.74	0.849	
	4.501.355	5 1.53	30	3.36	3.32	10.93	1.424	0.424	6001.5	0.205	0.164	0.060	0.033	201.5	7.08	-0.032	16.66	0.955	
<u></u>	5.001.907	_	_	3.30	3.15		1.582	0.471	8582.9	0.230	0.197	0.086	0.078	320.1	6.95	-0.050	11.65	1.062	
·-	5.502.365	_	40	3.22	3.01	13.36	1.740	0.518	10701.2	0.250	0.210	0.107	0.097	439.0	6.78	-0.048	9.34	1.160	Γ
	6.002.54		-	3.10	2.91	14.57 1.090	_	0.565	11469.4	0.235	0.195	0.115	0.104	\$13.3	6.53	-0.036	17.9	1.274	
	6.502.604		- 30	2.98	2.83	15.79	2.057	0.612	11636.3	0.213	0.173	911.0	0.104	563.2	6.20	-0.024	65.9	1.380	Γ
-	7.00 2.645	-4		2.85	2.73	17.00	17.00 2.215	0.660	11,724.7	0.195	0.156	0.117	0.104	612.2	6.30	-0.012	6.53	1.4:6	
	7.50 2.600	_		2.75	2.63	18.22	2.373	90. 0	11.771.1	0.178	0.129	0.118	0.103	658.5	5.75	0.0	1.50	1.592	
•	0.002.716	-	-+	2.63	2.52	19.43	2.532	0.754	11833.3	0.166	0.127	0.118	0.102	706.2	5.54	0.012	9.45	1.699	
•	8.50 2.770	-+		2.53	2.43	20.65		0.001	11978.6	0.156	0.117	0.120	0.102	759.5	5.33	0.024	1.35	1.805	
	9.002.822	-		2.43	2.34	21.86		0.848	12117.3	0.148	0.109	0.121	0.103	113.5	5.12	0.039	9.25	1.911	
•	9. 50 2. 869	-+	-	2.34	2.27			0.895	12379.3	0.140	0.104	0.124	0.104	6.77.3	4.93	0.051	8.08	2.017	
<u>.</u>	10.002.924	-+		2.27	2.22		3.165	0.942	12379.2	0.133	9.450	0.124	0.102	923.2	4.78	0.060	80°B	2,123	
	11. 30 2. 973	_	-	2.16	2.17	26.72	3.481 1.036	1.036	12355.0	0.117	7.946	0.124	0.099	0.009 1013.6	4.55	0.0	8.09	2.336	
	12.00 2.967	_	-	2.07	2.05	29.15	3.797	1.130	12126.6	0.103	6.567		0.093	0.093 1085.5	4.36	0.097	1.25	2.548	
	13.00 3.013		-	1.98	1.97	31.58		1.225	11969.4	9.300	ı	0.120	0.088	0.000 1160.7	4.17	0.10\$	8.35	7.761	
	14.00 3.020	_	•	1.92	1.92	34.01	Ē	1.319	11686.9	9.289				0.082 1220.5	4.04	0.112	8.56	2.973	
2	15.00 3.093	_1	4.73 +1.00	•	9.1	36.44	4.747 1.413	1.4	11760.1					0.079 1315.9	3.00	0.121	05.8	3.165	
	16.00 3.163	_	4.43  +1.02	1.76	7.80	38.87	38.87 5.064 1.507	1.507	11837.9	7.255	3.579	9.118	0.077	0.077 1412.9	3.71	0.123	\$7.8	1.398	

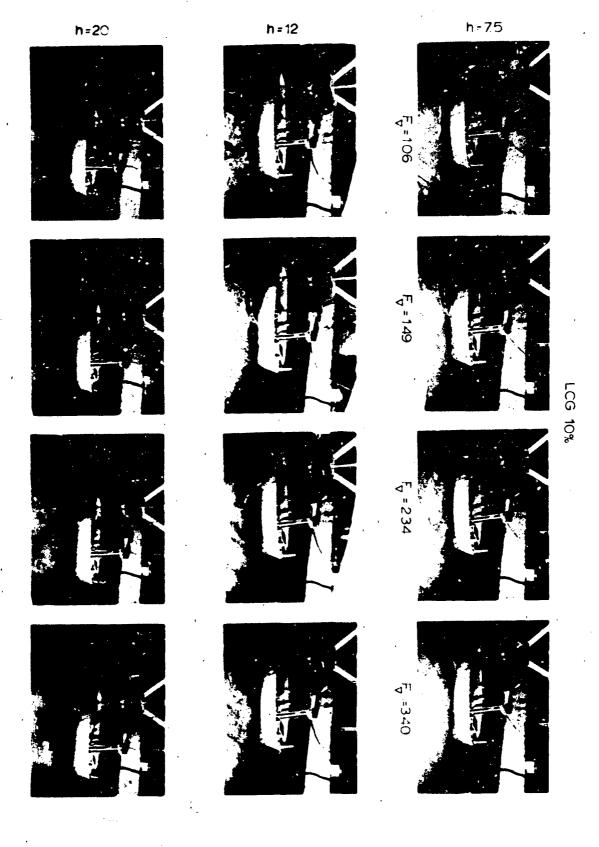
					_		780	•	200		1, 226	1, 337		1.560	1.671	1.783	1.694	2.006	2.117	2.229	2.452	2.675	2.897	3.120	3.343	7
ā					년	1			-			-	-		F	Ŀ	-	~	7	2	~	2.	~	5	_	1 566
100,000 11	0.000	A.T.T.C.		L	<b>&gt;</b>				_	-Ł	1.168	1.274	180	1.436	1.592	1.699	1.805	1.911	2.017	2.123	2.336	2.548	2.761	2.973	3.185	200
	•	4				16.00	25.81	10.17	**	9.74	10.33	10.34	10.33	10.04	9.90	9.79	9.78	9.72	9.70	89.6	9.38	9.20	9.07	9.13	8.94	8.84
CEMENT	LLOWING	LINE		RISE	40	-0.027	-0.054	-0.080	-0.030	0.024	0.027	0.024	0.025	0.033	0.039	0.046	0.054	0.060	0.064	0.06>	0.07	0.087	0.099	0.105	0.115	0.121
SHIP DISPLACEMENT	ROUGHNESS ALLOWANCE	PRICTION LI		S	\ \ \ \ \		6.95	6.9	6.78	6.53	6.26	6.11	5.92	5.75	5.56	5.29	5.08	4.87	4.70	4.53	4.25	4.09	3.96	4.06	3.79	3.74
SHIP	BOUG	PRIC		α.	و لنا	41.2	101.1	293.4	378.9	38	398.0	433.0	469.2	520.1	565.0	609.7	648.6	6.069	730.4	770.3	874.8	973.3	1069.1	1144.4	1251.7	1350.0
	•	\$×10-4		R		0.015	0.035	0.093	0.106	0.095	0.088	0.086	0.085	0.086	0.086	0.087	0.085	0.085	0.084	0.083	0.083	0.082	0.080 1069.	0.074 1144.4	0.074 1251.7	0.071 1350.0
68.0°F	1.9364		In	RA		0.01	0,039	0.098	0.113	0.1(3	0.097	0.097	0.097	0.100	0.101	0.102	0.102	0.103	0.103	0.103	0.107	0.109	0.110	0.110	0.112	0.113
TEMPERATURE :	•		E	Ú	x10-1	0.113	0.179	0.367	0.342	0.257	0.206	0.174	0.150	0.135	0.122	0.113	0.103	9.529	6.740	8.076	7.164	6.190	5.314	4.121	3.854	3.285
TEMPE				را ان	×10-1	12	0.222	0.410	0.384	0.298	0.247	0.214	0.190	0.175	0.162	0.152	0.142	0.134	0.126	0.119	0.110	6.6	9.083	7.858	7.551	6.954
101	3.50 ft	16.84		کا	<u>S</u> 4	1840.3	3072.0	9833.3	11289.1	10263.1	9701.3	9675.3	9677.1	9960.2	10098.8	10217.1	10228.7	10291.7	10306.8	10326.6	10661.0	10873.4	11024.3	10958.4	11186.6	11310.8
•		=		IL.	=	0.282	0.329	0.377	0.424		0.518	0.565	0.612	0.660	0.706	0.754			0.895	745	1.036	7.730	1.225	1.319		1.507
L.C.G. LOCATION	RIGHT	ALE RATIO		>[	7	0.945	1.107	1.266 0.377	1.424			1.898	2.057 0.612	2.215		2.532	20.65 2.690	- 1		3.105	3.481		4.114	4:431	4.747	8.87 5.064 1.507
L.C.G.	HODEL LENGTH	SCALE 1		>		7.29	8.50	9.71	10.93	-	_1	긔	15.79		7			1	7   "						7	7
				۾ لــــ	g =	3.25	3.37	3.25	3.07	2.95	2.16	2.7	2.68	2.58	2.51	2.44	2.36	2.27	2.22	1:1	2.07	2.00	1.93	8 1	1:86	1.82
		136		S	ft.2	3.1	3.36	3.32	3.23	3.10	2.97	2.90	2.81	2.73	2.64	2.51	7.5	2.31	2.23	ç;;	2.05	1.94	1.88	2	9	
17.0	10-75	1 16 Pab. 1969		ပ္ပ		23	45	55	25	+.20	4.22		+.21	_1	+.32	B		L		/6.	÷ ;	7/:-	÷.82	+.87	c	3.83 1+1.00
				8	degree inch	1.28	1.33	3.13	4.73		4.23	- 1	- 1	4.63	4.93	5.23	5.43	50.0	5.83	2.33	5.83	50.0	5.13	4.63	57.	20.5
MODEL NO. : 1174	TEST NO.	DATE		2	1b	. 436	. 972	4.00 2.11	4.50 2.429	5.00 2.242	5. 50 2. 149	6.00 2.167	6.50 2.194	7.00 2.278	0 00 2.331	0.00 2.3/5	9. 30 2. 400	9 50 2 435	10.00 2 488		12 00 2 203	6. /06	7. / 34	15 00 2 878	16 00 2 063	3.083
<b>=</b>	-			>	fps	3.00	3.50	00.	2	8	2	8	6.50	2.0	200	9 6	9 6	3	10	1	2		13.00 2. /94	30 5	16 00 2 063	
																					•					

1.6 page   1.00   1.						_	2	12	2	2	2	3	36	3	32	20	18	3	3	72		36	12	=	3	9	ŀ
The part of the p	ē				u	<u> </u>	-	•	·		•	į	-	=	1.2	E	-	-	-	7.6	1.7	F	2	2.2	7.7	2.640	•
The part of the p	000,	960	r. r.c.		L	<b>&gt;</b>	0.637	0.743	9.849	0.955	1.062	1.168	1.274	1.380	1.406	1.592	1.699	1.005	1.911	2.017	2.123	2.336	2.548	2.761	2.973	3.185	1
The part of the p	91 -		. A.			Δ.	\$5.70	+	20.03	12.30					9.57	9.40		9.10	9.10	9.06	.91	11:	9.90	6.77	19.8	97.9	36.
1. 16 Pab. 1969 SCALE MATO 1. 16.04 WEEPERATURE 1. 6.00 Part 1.00 Part 1.00 Part 1. 15.04 Pab. 1960 SCALE MATO 1. 16.04 WATER DEFTH = 12.0 in. 0.10000810^4 Part 1. 16.04 Part 1. 12.0 in. 0.1000810^4 Part 1. 16.04 Part 1. 12.0 in. 0.10091 Part 1. 12. 0. 12. 0.10091 Part 1. 12. 0.10091		ONANCE			SE	\$2	5.00	9.010	0.036	┺	0.073	0.0	0.042	0.036	9.019	0.015	0.035	0.042	0.054	0.060	0.066	6.677	0.065	0.093	0.103	0.114	161 0
1. 16 Pab. 1969 SCALE MATO 1. 16.04 WEEPERATURE 1. 6.00 Part 1.00 Part 1.00 Part 1. 15.04 Pab. 1960 SCALE MATO 1. 16.04 WATER DEFTH = 12.0 in. 0.10000810^4 Part 1. 16.04 Part 1. 12.0 in. 0.1000810^4 Part 1. 16.04 Part 1. 12.0 in. 0.10091 Part 1. 12. 0. 12. 0.10091 Part 1. 12. 0.10091	ISPLACE	PSS ALL	ON LIMI		S	\$2		6.80	7.06	- 66 . 9	6.78 -	<u>.                                    </u>	L	<u> </u>		<u> </u>	_			L_		<u> </u>	١	1	<u> </u>	<u> </u>	3 66
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	MIP D	OUGHN	RICTI				上		7:	L	•	1_	L	-	L	•	0.	1.	•	•	9.0	5:	•	_	_	L	L
CC CG S L V K LITTA I 16.00 LINER I 100 LINER DEPTH = 13.0 ft LINE	<b>4</b>	*	<u> </u>				L	<u> </u>		L		ŀ	L_	乚	<u> </u>				_		_	L_	1005	1100	1105	1275	0 081 1427 6
1. 16 Pab. 1969 SCALE PATIO : 16.04 PROPERATURE : 60.090 PATIO : 16.04 PATIO : 16.04 PATIO : 10.000 PATIO : 10			01×0		R R	V	6.61	0.029	0.043	0.074	0.119	0.117	0.100	0.09	0.091	0.091	0.092	60.0	0.091	0.090	0.090	0.0	0.0	0.08	0.080	0.37	0.0
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC	68.0°F	1.9364	0.1080	12.0 1	RTS	1	9.618	0.039	9.048	0.081	0.127	0.126	0.111	0.106	0.10\$	0.106	0.108	0.110	0.110	0.110	0.111	0.113	0.112	0.114	0.114	0.114	0.120
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC	ATURK :				رن ن	×1-01	0.110	0.134	0.166	0.231	0.311	0.260	0.193	0.158	0.138	0.125	0.114	901.0	9.709	996.8	8.338	7.179	6.093	5.336	4.615	3.988	3.9.33
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC	TENDRO			MATER.	را		0.155	0.177	0.209	0.273	0.352	0.300	0.233	0.196	0.178	0.164	0.153	0.145	0.136	0.128	0.122	0.110	9.882	9.101	1381	7.704	7.328
CCCCCTION: INDEL INNITH INDEL INDEL INNITH INDEL INNITH INDEL INNITH INDEL INDEL INNITH INDEL INDEL INNITH INDEL INDEL INNITH INDICED IN INDEL INNITH INDICED INDEL INDEL INDEL INNITH INDICED INDEL INDEL INDEL INDICED INDEL INDICED INDEL INDICED INDEL INDICED INDICED INDICED INDICED INDEL INDICED INDIC		50 ft	:		2	n		2936.1	4800.7	8075.2	12734.1	12615.2	11116.3	10556.1	10447.5	10633.9	10792.0	10993.9	10991.2	11041.0	11135.4	11255.1	11237.4	11408.0	11354.8	11395.6	11961.6
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC	•		91 -		ئىدا	-	0.202	0. 329	775.0	0.424	0.471	0.510	0.565	0.612	0.660	907.0	0.754	0.801	0.348	0.395	0.942	1.036	1.130	1.225	1.319	1.413	1 507
1. 10-13   15.	OCAT 10	NCTH	.T10		>[	<u> </u>	1			1.424		1.740		2.057	2.215	2. 173		2.690	2.848	3.008		3.481			4.431	4.747	39.87 5.064 1.507
1. 10-13  1. 16 70	C.G. 1.	OKL LE	ALK RA	İ	>×	<u> </u>	7.29	0. ∶0	9.71		12.14		14.57	15.79	17.00	18.22	19.43	20.65	21.86	3.08		26.12	29.15	31.58	34.01	36.44	39.87
1. 11. 12. 13. 13. 13. 13. 13. 13. 13. 13. 13. 13	<u>.</u>	2	S		7	2 2	1.21	3.30	3.35	3.20	3.05	2.95	2.86	2.77	2.69	2.57	2.48	2.37	2.30	2.23	2.17	2.10	2.02	1.94	1.8	1.01	1.69
			1961	ĺ	S	Ct.	3.15	3.23	3.35	3.32	3.22	3.12	3.03	2.93	2.82	2.73	2.63	2.52	2.43	2.34	2.26	2.13	2.03	1.94	1.05	1.79	1.71
	174	-12	į		ဗ္ဗ		04	15	30	65	09	00.	+.35	+.30	+.16	+.22	+.29	+.35	+.45	+.50	+.55		+.70	+.77	+.85	*:	4.13 +1.00
PONE M PATE  THE TOP COLOR OF THE TOP C	0. 1 11		- i			dogree	+1.03	•6.9	1.33	+3.13	6.13	6.13	5.23	4.73	4.63	4.68	4.78	•	5.13	5.43	5.63	5./3			_	1	
2 2 3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	N 7360	ON ASS	ATE		2		1 1	.68	1.005	1.177	2.750	2.750	2.470	2.301	2.303	2.448	2.505	2.570	2.594	2.628	2.672	2.746	2.797	2.889	2.932	3.004	16.00 3.106
the state of the s	2	ب	٥		>2	tb3	3.00	3.50	1.00	1.30	5.00	5.50	.00	6.50	2.6	7.50	9.00	, e	9.00	٠. 5	-00	11.00	12.00	13.00	14.00	15.00	16.00

				الل ع		. 40	. 677	. 545	.613	.682	.750			.954	1.023	1.091	1.159	1.227	1.295	1.364	1.500	1.636	1.73	1.909	2.046	2.:82	
100,000 15	000	A.T.T.C.		<u>"</u>		0.637	0.743	0.849	0.955	1.062	1.168	1.274	1.330	1.436	1.592	1.699	1.805	1.911	2.017	2.123	2.336	2.548	2.761	2.973	3.185	3. 198	
-	0.000	. A.T	Ì			55.72	34.07	23.56	16.07	11.52	8.88	7.05	7.86	8.15	8.40	05.0	8.55	8.48	8.42	8.36	8.30	8.33	8.39	8.30	6.23	8.04	
ENERGY	LO:4ANCE	<b>2</b>		RISE	Λ <del>\$</del>	-0.004	-0.012	-0.024	6.99 -0.040	-0.057	-0.054	-0.042	-0.006	0.018	0.033	0.040	0.045	0.054	0.063	0.069	0.081	0.091	0.100	0.110	0.114	0.121	
SHIP DISPLACEMENT	HOUGHNESS ALLOWANCE	PRICTION LINE		S	<b>₹</b>	6.53	6.63	6.95	6.99	89.9	9.44	6.21	00.9	5.83	5.64	5.52	5.39	5.22	5.05	4.93	4.70	4.42	4.21	4.00	3.79	3.60	
BHIP	#OOG	FRIC		σμ	나 술	40.2	76.6	126.7	198.9	323.8	462.2	570.2	616.5	640.5	1.999	701.9	941.6	791.2	842.1	191.9	988.7	1074.6	1155.6	1258.5	1359.8	0.084 1483.7	
4.0.09		01×0	;	R R	V	0.015	0.025	0.037	0.052	0.079	0.103	0.117	0.115	0.109	0.104	<u> </u>	0.099	0.099	0.098	_	0.095	0.092		0.086	0.084		
	1.9364	n : 0.10808x10-4	20.0 in.	$R_{TS}$	Ø	0.018	0.039	0.042	0.059	0.087	0.113	0.127	0.127	0.123	0.119	<u> </u>	0.117	0.118	0.119	1_	0.121	0.120	0.119	0.120	0.122	0.124	
ATURE :	•	2	DEPTH =	ပ	X10-1X	0.112	0.137	0.147	0.164	0.209	0.234	0.231	0.201	0.169	0.145	0.127	0.112	0.103	9.523	8.739	1	6.365	5.441	4.838	4.347	4.012	
TEMPERATURE			MATER	C	x10-1-	1	0.101	0.189	0.208	0.250	0.275	0.271	0.241	0.209	0.185	0.166	0.151	0.141	0.133	0.125	0.112	0.101	9.185	8.567	8.066	7.722	
	3.50 ft	•		2	<u>s</u>	1794.6	2935.4	4244.8	5926.5	6600.3	11265.4	12740.8	12715.6	12267.0	11905.8	11762.6	11695.9	11785.9	11883.2	11956.6	12049.2	12005.1	11916.3	12050.9	12153.2	12431.2	
101 : MC	. 3	16.84		L		0.282		0.377	0.424	0.471	0.518	0.565	0.612	0.660	0.766	0.754	0.801	0.848	0.395	0.942	1.636	1.130	4.114 1.225	4.431 1.319	4.747 1.413	1.507	
.G. LOCATION	EL LENGTH	WTIO		>[	٢	0.945		9.71 1.266 0.377	1.424	1.582	13. 36 1. 740 0.518	1.898		17.00, 2.215	18.22 2.373	19.43 2.532	20.63 2.690	21.86, 2.848	23.08 3.006	24.29 3.165	26.72 3.481	5 3.797		1		38.87 5.064 1.507	
1.0.6.	NOORL 1	SCALE RATIO		>		7.29	4	_	10.93	12.14	<u> </u>	+	-	+-	-	4-	+-	<del>-</del>	┪	<b>-</b>		8 29.15	0 31.58	0 74.01	0 36.44	-	
					ਨੇ ± 	3.19	4-	1.37		4			<del>-</del> -	7 2.65	<del></del> -	┿	-	<u> </u>	-	┵	<u> </u>		+	0 1.90	-	1.71	
MODEL NO. : 1174		1969		S	ي م			. 1	. 1	+	-		-	┵-	-	+-	∔-	_	4	+		+-	<del></del>	1.90	-	11.11	
	10-20	: 22 Feb. 1969	,	18		.03		- 20	4-	<u> </u>	-	<del>-   -</del>	+	+	- +			_	<del></del>	-}	- +	-	<u> </u>	+.91	+	4.43 +1.00	;
	٦ •		,	8	ASIST CONTRACTOR	1.33	1.23	1	ł	3.03					5	2 6		┷	_	6.43	6.33	6.03	+-	4	4		
	WEST NO.	DATE		2	Σ	426	1			5.00 1 622	5.502.472	6 00 2 796	6.502 815	7 00 7	7 50 2 70	8 00 2 701	8 30 2 716	9.00 2.760	9 :012 804	10.00 2 848	11 00 2 925	12.002.968	13.003.006	14.00 3.089	15.0013.163	16.00 3.273	j
×	;	ă		>	Σ			8	4.50	\$	50	9	6.50	8	2.50	9	8	90	6	10	1	0 7	100	1	1.5	16.0	







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